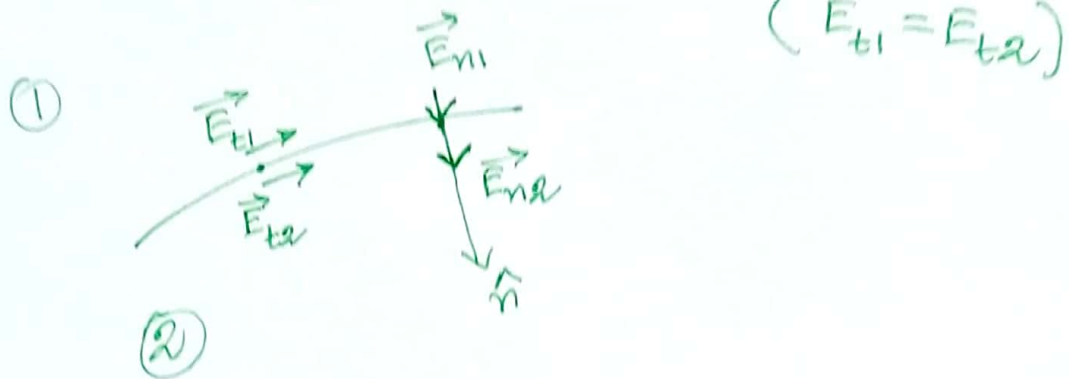


Recap of boundary conditions of \vec{E} and \vec{H} :

- Tangential components of \vec{E} is continuous across an interface between two media.



- Normal components of \vec{D} are discontinuous by an amount σ , the surface charge density at the interface. i.e. $(D_{n2} - D_{n1}) = \sigma_{\text{surface}}$

If surface charge is zero,

$$D_{n2} = D_{n1}$$

$$\Rightarrow \epsilon_2 E_{n2} = \epsilon_1 E_{n1}$$

- Normal components of \vec{B} are continuous across the interface. $B_{n2} = B_{n1}$

- Tangential components of \vec{H} are discontinuous by an amount \vec{K} , the surface current density.

$$H_{t2} - H_{t1} = K$$

For a perfect dielectric (conductivity = 0),

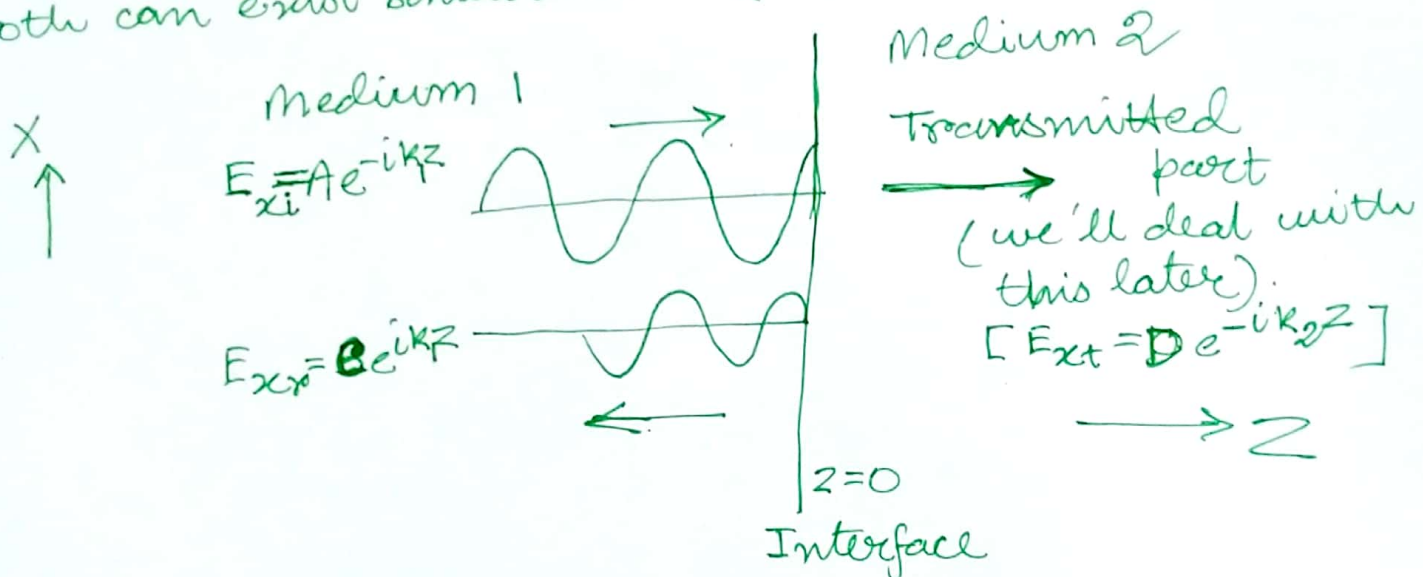
$$H_{t2} = H_{t1}$$

- We also learnt that electromagnetic field can not exist inside a perfect conductor. So, when an e.m. wave strikes a conducting (to be precise, perfectly conducting) surface, the entire energy is reflected back.

(1)

Travelling and standing wave:

Recall: we solved 1D Helmholtz equation and saw that two solutions are possible. One is Be^{ikz} (wave travelling along $-z$ direction and the other one is Ae^{-ikz} (wave travelling along $+z$). We considered only one of these two candidates so far. But in general, both can exist simultaneously:



(X-polarized ~~plane~~ plane wave incident at a planar interface between two dielectric media)

Total \vec{E} -field in medium 1:

$$E_{x1} = Ae^{-ik_1z} + Ce^{ik_1z} \quad (1)$$

Total \vec{H} -field in medium 1:

$$H_{y1} = \frac{1}{\eta_1} (Ae^{ik_1z} - Ce^{ik_1z})$$

$[\eta_1 = \text{intrinsic impedance of medium 1}]$

$$\eta_1 = \sqrt{\frac{\mu_1}{\epsilon_1}}$$

We are omitting the time dependence for ease of writing.

But always remember, the actual field is:

$$E_{x1}(z, t) = E_{x1}(z) e^{i\omega t} = Ae^{i(\omega t - k_1z)} + Ce^{i(\omega t + k_1z)}$$

(2)

How will the function E_{x1} in eq. (1) look like?

Let's try to write it in a form:

$$E_{x1} = r e^{-i\theta}$$

$$\Rightarrow A e^{-i k_1 z} + C e^{i k_1 z} = r e^{-i\theta}$$

$$\Rightarrow (A+C) \cos(k_1 z) - i(A-C) \sin(k_1 z) = r \cos \theta - i r \sin \theta$$

Equate real and imaginary parts:

$$r \cos \theta = (A+C) \cos(k_1 z) \quad \text{--- (3)}$$

$$r \sin \theta = (A-C) \sin(k_1 z) \quad \text{--- (4)}$$

$$\therefore \tan \theta = \left(\frac{A-C}{A+C} \right) \tan(k_1 z)$$

$$\Rightarrow \theta = \tan^{-1} \left[\left(\frac{A-C}{A+C} \right) \tan(k_1 z) \right] \quad \text{--- (5)}$$

$$\text{and } r = \sqrt{(A+C)^2 \cos^2(k_1 z) + (A-C)^2 \sin^2(k_1 z)}$$

$$= \sqrt{A^2 + C^2 + 2AC \cos^2(k_1 z) - 2AC \sin^2(k_1 z)}$$

$$= \sqrt{A^2 + C^2 + 2AC \cos(2k_1 z)}$$

$$\therefore E_{x1} = r e^{-i\theta} = \sqrt{A^2 + C^2 + 2AC \cos(2k_1 z)} \cdot e^{-i \tan^{-1} \left\{ \left(\frac{A-C}{A+C} \right) \tan(k_1 z) \right\}}$$

$$|E_{x1}| = \sqrt{A^2 + C^2 + 2AC \cos(2k_1 z)}$$

↑ Known as standing wave pattern.

$$|E_{x1}|_{\max} = \sqrt{A^2 + C^2 + 2AC} = (A+C)$$

↳ Occurs at $(2k, z) = 2n\pi$

$[n=0, \pm 1, \pm 2, \dots]$

$$\Rightarrow k, z = n\pi$$

$$\Rightarrow \frac{2\pi}{\lambda_1} z = n\pi$$

$$\Rightarrow z = n \cdot \left(\frac{\lambda_1}{2}\right)$$

$$|E_{x1}|_{\min} = \sqrt{A^2 + C^2 - 2AC} = (A-C)$$

↳ Occurs at $(2k, z) = (2n+1)\pi$

$[n=0, \pm 1, \pm 2, \dots]$

$$\Rightarrow k, z = \left(n + \frac{1}{2}\right)\pi$$

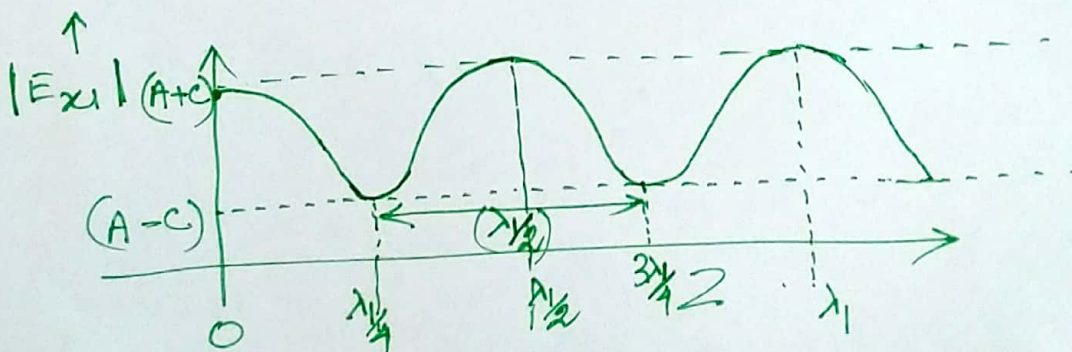
$$\Rightarrow \frac{2\pi}{\lambda_1} z = \left(n + \frac{1}{2}\right)\pi$$

$$\Rightarrow z = \left(n + \frac{1}{2}\right) \left(\frac{\lambda_1}{2}\right)$$

Also, $|E_{x1}|$ is periodic ^{in z} with a periodicity ~~$\frac{\lambda_1}{2}$~~ $\left(\frac{\lambda_1}{2}\right)$.

$$2k, z =$$

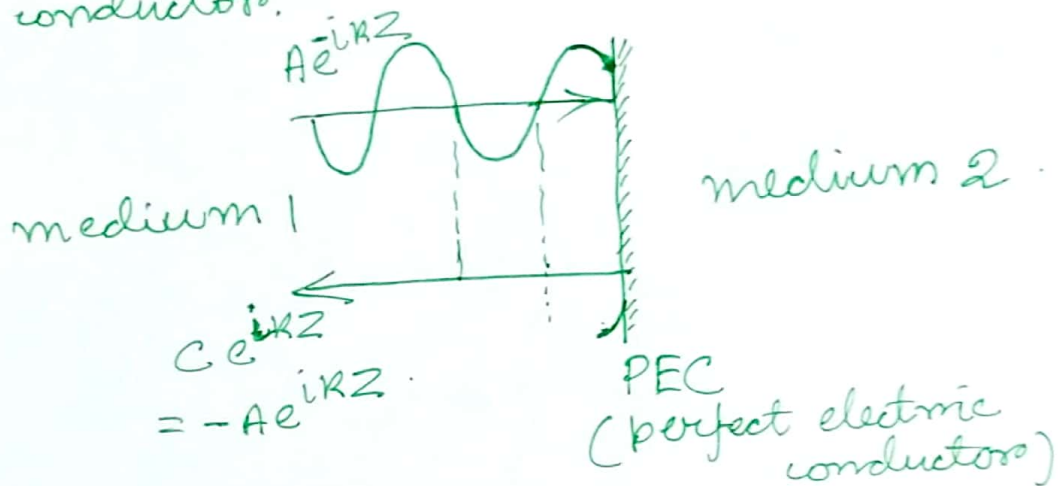
[can be easily seen noting that the distance between consecutive maxima and minima are $\left(\frac{\lambda_1}{2}\right)$]



(4)

Suppose, instead of choosing medium 2 to be a dielectric, we let it be a perfect conductor. Alternate arrangement; we put a perfect conductor at the interface between two dielectric media.

Both of these above arrangements will give rise to the same effect in medium 1 \Rightarrow the entire incident energy must be reflected back to medium 1. Because: e.m. wave cannot penetrate perfect conductor.



$$\therefore E_{x1} = A e^{-i k_1 z} - A e^{i k_1 z}$$

$$= -2iA \sin(k_1 z)$$

$$E_{x1}(z, t) = -2iA \sin(k_1 z) e^{i\omega t}$$

$$H_{y1} = (A e^{-i k_1 z} + A e^{i k_1 z}) \cdot \frac{1}{\eta_1}$$

$$= \frac{2A}{\eta_1} \cos(k_1 z)$$

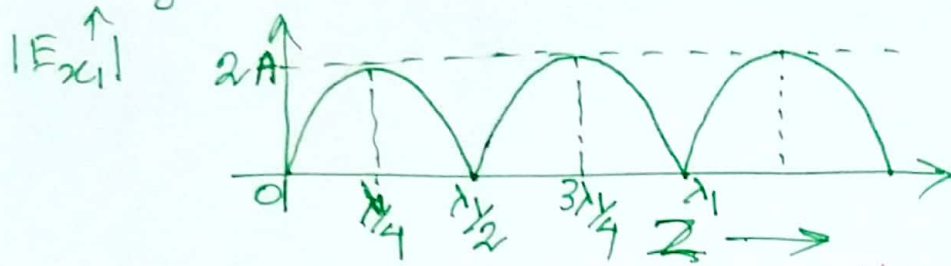
$$H_{y1}(z, t) = \frac{2A}{\eta_1} \cos(k_1 z) e^{i\omega t}$$

The time averaged Poynting vector

$$= \text{Real} \left\{ \vec{E}_{x1} \times \vec{H}_{y1}^* \right\} = 0 \quad \left[\text{Note the phase difference between } E_{x1} \text{ and } H_{y1} \text{ due to presence of } i \right].$$

(5)

In other words, if $A = -C$, there is no net flow of energy averaged over time. This is the reason, the case of the superposition of equal amount of incident and reflected wave, is known as a pure standing wave.



Standing wave pattern of a pure standing wave.

The standing wave pattern tells you how much is the content of "pure standing wave" in a given waveform: if the minima is at zero field (i.e. $|E_x| = 0$) the wave is a pure standing wave (no time averaged energy flow). An increase in A decreased difference between field maxima and minima values would denote progressively smaller value of C , the reflected wave. Thus, the standing wave content in the waveform decreases. A flat standing wave pattern means $C = 0$. In other words difference between $|E_x|_{max}$ and $|E_x|_{min}$ is zero [$|E_x|_{max} = |E_x|_{min} = A$].

So, no reflected wave at all. Meaning that no standing wave content in the waveform.

The ratio $\frac{|E_x|_{max}}{|E_x|_{min}}$



is called standing wave ratio (SWR).

Maximum value of SWR occurs for a pure standing wave, since $|E_x|_{min} = 0$. So, $SWR_{max} \rightarrow \infty$
 Minimum SWR occurs when we have a pure

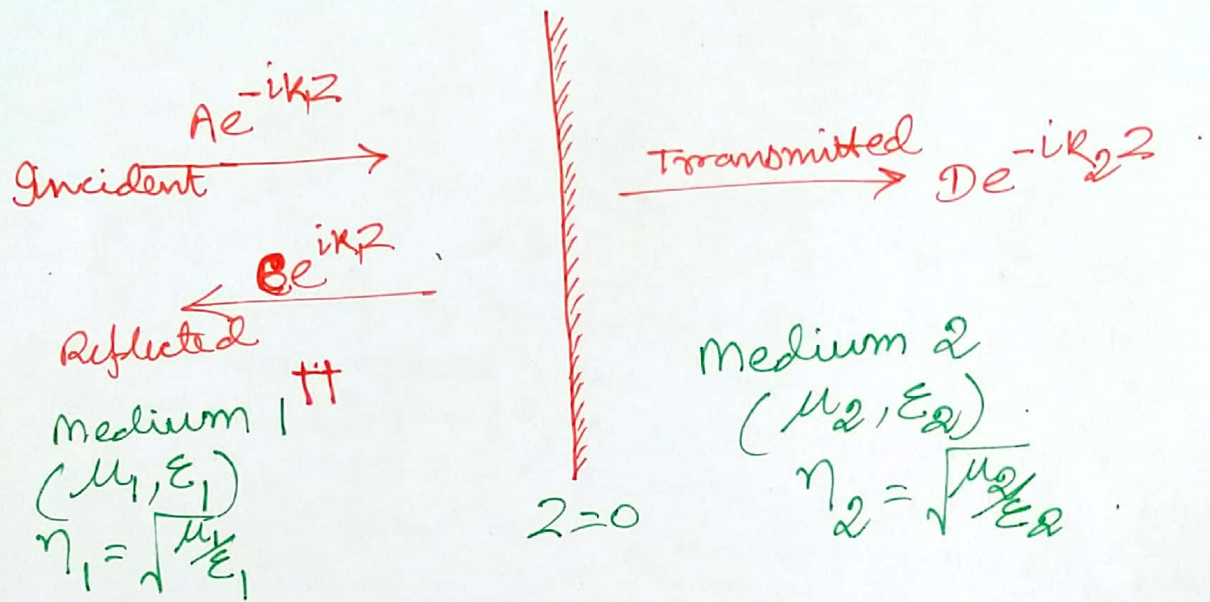
travelling wave i.e. $|E_x|_{\max} = |E_x|_{\min}$

So, $(\text{SWR})_{\min} = 1$.

This is a very important property of SWR:

$$1 \leq (\text{SWR}) < \infty$$

Reflection of E.M. wave at a planar interface



$$E_{x1} = Ae^{-ik_1z} + ce^{ik_1z} \quad \text{--- (6)}$$

$$E_{x2} = De^{-ik_2z} \quad \text{--- (7)}$$

Let us define a quantity Γ_z as reflection coefficient. Γ_z is a complex number and is the ratio of the amplitude of the reflected to the incident \vec{E} -field.

$$\therefore \Gamma_z = \frac{ce^{ik_1z}}{Ae^{-ik_1z}} = \frac{c}{A} e^{i2k_1z}$$

$$|\Gamma_z|_{z=0} = \frac{c}{A} = \Gamma$$

$$\therefore \Gamma_z = \Gamma e^{i2k_1z} \quad \text{--- (8)}$$

[Note that $\Gamma = |\Gamma_z|$]

Imp:
These media can be conductive, the same formulation will be applicable just by replacing ϵ_1 and ϵ_2 by effective complex $\epsilon_{1\text{eff}}$ and $\epsilon_{2\text{eff}}$.

Similarly, we define a transmission coefficient T as the ratio of the transmitted field amplitude to the incident field amplitude at the interface.

$$\therefore T = \frac{D}{A}$$

Thus eqns. (6) and (7) can be written as:

$$E_{x1} = A [e^{-ik_1 z} + \Gamma e^{ik_1 z}] \quad \text{--- (9)}$$

$$\text{and } E_{x2} = AT e^{-ik_2 z} \quad \text{--- (10)}$$

The expressions for the magnetic fields will be:

$$H_{y1} = \frac{A}{\eta_1} [e^{-ik_1 z} - \Gamma e^{ik_1 z}] \quad \text{--- (11)}$$

$$H_{y2} = \frac{AT}{\eta_2} e^{-ik_2 z} \quad \text{--- (12)}$$

At this point, let's make an important observation:
 Irrespective of angle of incidence, E_x and H_y components are always tangential to the interface at $z=0$. According to the boundary conditions ~~at a pure dielectric~~ they must be continuous across the interface.
 Thus, the ratio $E_x/H_y = \eta_2$ must also be continuous across the interface.

$$\eta_2 \Big|_{z=0} = \eta_2 \Big|_{z=0} \quad \left[\text{This is coming from:} \right]$$

$$\frac{E_{x1}}{H_{y1}} \Big|_{z=0} = \frac{E_{x2}}{H_{y2}} \Big|_{z=0}$$

$$\Rightarrow \frac{A(1+\Gamma)}{\frac{A}{\eta_1}(1-\Gamma)} = \eta_2$$

$$\Rightarrow \frac{1+\Gamma}{1-\Gamma} = \eta_2 / \eta_1 \Rightarrow \boxed{\Gamma = \left(\frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} \right)} \quad \text{--- (13)}$$

From the continuity equation of E_{x1} and E_{x2} at $z=0$,
 $A(1+\Gamma) = AT$ [put $z=0$ in eqns (9) and (10)]

$$\Rightarrow \boxed{T = 1 + \Gamma} \quad \text{--- (14)}$$

$$\therefore T = 1 + \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} = \left(\frac{2\eta_2}{\eta_1 + \eta_2} \right) \quad \text{--- (15)}$$

- At this point we would like to write SWR in a nicer way:

$$SWR = \frac{|E_{x1}|_{\max}}{|E_{x1}|_{\min}} = \frac{A+C}{A-C} = \frac{1+|\Gamma|}{1-|\Gamma|}$$

- If both media (1) and (2) are non-magnetic [i.e. $\mu_1 = \mu_2 = \mu_0$], the expressions for Γ and T can be further simplified as:

$$\Gamma = \frac{\sqrt{\frac{\mu_0}{\epsilon_2}} - \sqrt{\frac{\mu_0}{\epsilon_1}}}{\sqrt{\frac{\mu_0}{\epsilon_2}} + \sqrt{\frac{\mu_0}{\epsilon_1}}} = \left(\frac{\sqrt{\epsilon_1} - \sqrt{\epsilon_2}}{\sqrt{\epsilon_1} + \sqrt{\epsilon_2}} \right) = \left(\frac{n_1 - n_2}{n_1 + n_2} \right)$$

$$T = \frac{2\sqrt{\frac{\mu_0}{\epsilon_2}}}{\sqrt{\frac{\mu_0}{\epsilon_1}} + \sqrt{\frac{\mu_0}{\epsilon_2}}} = \frac{2\sqrt{\epsilon_1}}{\sqrt{\epsilon_1} + \sqrt{\epsilon_2}} = \frac{2n_1}{n_1 + n_2}$$

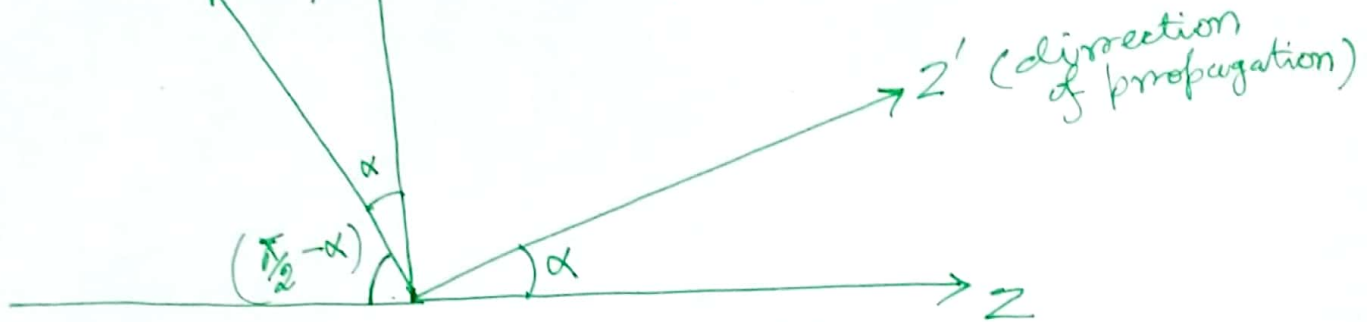
Here, $n_1 = \sqrt{\frac{\epsilon_1}{\epsilon_0}} = \sqrt{\epsilon_{r1}}$ } definition of refractive indices of the media.
 $n_2 = \sqrt{\frac{\epsilon_2}{\epsilon_0}} = \sqrt{\epsilon_{r2}}$ } [i.e. in general, r.i. (n)
 $= \sqrt{\epsilon_r} = \sqrt{\frac{\epsilon}{\epsilon_0}}$]

Uniform plane wave at an interface — Oblique incidence

Before we continue to the case of oblique incidence, we 'll need some tools in our hand. The problem statement of this introductory part is very simple:

How do we represent a ~~plane~~ uniform plane wave that travels along a direction z' , where z' makes an angle α with z ?

(x is directed into the paper-plane)



$$z' = (z \cos \alpha + y \sin \alpha) \quad \text{--- (16)}$$

Let \hat{y}' be the unit vector along y' axis.

$$\therefore \hat{y}' = (\hat{y} \cos \alpha - \hat{z} \sin \alpha) \quad \text{--- (17)}$$

Possibility 1: \vec{E} is parallel to $z=0$ plane i.e. along x direction and \vec{H} is along y' .

$$\vec{H} \quad E_x = A e^{-ikz'} = A e^{-ik(z \cos \alpha + y \sin \alpha)} \quad \text{--- (18)}$$

$$\vec{H} = \hat{y}' \frac{A}{\eta} e^{-ikz'}$$

$$\Rightarrow \vec{H} = (\hat{y} \cos \alpha - \hat{z} \sin \alpha) \frac{A}{\eta} e^{-ik(z \cos \alpha + y \sin \alpha)}$$

[From eqn (17) and (18)]

$$\text{--- (19)}$$

$$\therefore H_y = \frac{A}{\eta \cos \alpha} e^{-ik(z \cos \alpha + y \sin \alpha)} \quad \text{--- (20)}$$

We obtain the 2-directed impedance, $\eta_2 = \frac{E_x}{H_y}$ as:

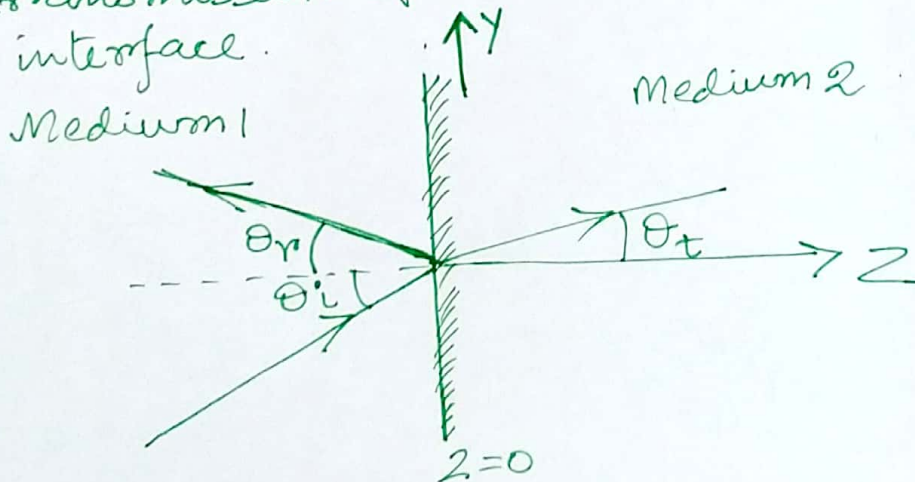
$$\eta_2 = \left(\frac{\eta}{\cos \alpha} \right) \quad \text{--- (21)}$$

Possibility 2: \vec{H} is parallel to $z=0$ plane i.e. along x and \vec{E} is along y !

$$\begin{aligned} \therefore H_x \neq 0 \quad \therefore \vec{E} &= \hat{y}' A e^{-iKz'} \\ &= (\hat{y} \cos \alpha - \hat{z} \sin \alpha) A e^{-iK(z \cos \alpha + y \sin \alpha)} \\ H_x &= -\frac{A}{\eta} e^{-iKz'} = -\frac{A}{\eta} e^{-iK(z \cos \alpha + y \sin \alpha)} \end{aligned}$$

$$\therefore \eta_2 = -\frac{E_y}{H_x} = \eta \cos \alpha \quad \text{--- (22)}$$

Now is the time for the real problem of reflection and transmission of an e.m. wave incident obliquely at an interface.



The interface is the $z=0$ plane. θ_i , θ_r and θ_t are angles of ~~reflection~~, incidence, reflection and transmission (you may call it refraction), respectively.

First, we'll consider the case 1 (i.e. \vec{E} parallel to the interface and along X direction).

- ① For the incident wave, $\alpha = \theta_i$.
- ② For the reflected wave, $\alpha = (\pi - \theta_r)$
- ③ For the refracted wave, $\alpha = \theta_t$.

$$\therefore E_{xi} = A e^{-ik_1(2\omega z \theta_i + y \sin \theta_i)} \quad \text{--- (23)}$$

[from eqn (18)]

$$E_{xr} = A \Gamma e^{-ik_1(-2\omega z \theta_r + y \sin \theta_r)} \quad \text{--- (24)}$$

$$E_{xt} = A T e^{-ik_2(2\omega z \theta_t + y \sin \theta_t)} \quad \text{--- (25)}$$

Now, $E_{xi} + E_{xr} = E_{xt}$ at $z=0$, *for all y.*

$$\therefore A e^{-ik_1 y \sin \theta_i} + \Gamma A e^{-ik_1 y \sin \theta_r} = A T e^{-ik_2 y \sin \theta_t}$$

If the above equation is valid for all y, *for all y.*

$$k_1 \sin \theta_i = k_1 \sin \theta_r = k_2 \sin \theta_t$$

$\therefore \boxed{\theta_i = \theta_r}$ — You have seen this!
Law of reflection.

And,

$$k_1 \sin \theta_i = k_2 \sin \theta_t$$

$$\Rightarrow \omega \sqrt{\mu_1 \epsilon_1} \sin \theta_i = \omega \sqrt{\mu_2 \epsilon_2} \sin \theta_t$$

$$\Rightarrow \frac{\sin \theta_i}{\sin \theta_t} = \sqrt{\frac{\mu_2 \epsilon_2}{\mu_1 \epsilon_1}}$$

If the media are non-magnetic ($\mu_1 = \mu_2 = \mu_0$)

$$\frac{\sin \theta_i}{\sin \theta_t} = \sqrt{\frac{\epsilon_2}{\epsilon_1}} = \sqrt{\frac{\epsilon_{20}}{\epsilon_{10}}} = \frac{\sqrt{\epsilon_{20}}}{\sqrt{\epsilon_{10}}} = \frac{n_2}{n_1}$$

— Snell's law!!

Also, $H_{y1} = H_{yi} + H_{yr}$

$$= \omega_3 \theta_i \frac{A}{\eta_1} \left(e^{-ik_1 z \omega_3 \theta_i} - \Gamma e^{+ik_1 z \omega_3 \theta_i} \right)$$

[we have deliberately dropped the y-variation here since ultimately it's same for all 3 and ~~going~~ going to get cancelled]

$$H_{y2} = \omega_3 \theta_t \frac{A}{\eta_2} e^{-ik_2 z \omega_3 \theta_t}$$

$$\left. \frac{E_{x1}}{H_{y1}} \right|_{z=0} = \left. \frac{E_{x2}}{H_{y2}} \right|_{z=0} \quad [\text{2-directed impedances at the interface must be equal}]$$

$$\Rightarrow \frac{A(1+\Gamma)}{A \frac{\omega_3 \theta_i}{\eta_1} (1-\Gamma)} = \frac{\eta_2}{\omega_3 \theta_t} \rightarrow \text{This part is known from eqn. (21)}$$

$$\Rightarrow \frac{\eta_1}{\omega_3 \theta_i} \left(\frac{1+\Gamma}{1-\Gamma} \right) = \frac{\eta_2}{\omega_3 \theta_t}$$

$$\Rightarrow \frac{1+\Gamma}{1-\Gamma} = \frac{\left(\frac{\eta_2}{\omega_3 \theta_t} \right)}{\left(\frac{\eta_1}{\omega_3 \theta_i} \right)}$$

$$\Rightarrow \Gamma = \frac{\left(\frac{\eta_2}{\omega_3 \theta_t} - \frac{\eta_1}{\omega_3 \theta_i} \right)}{\left(\frac{\eta_2}{\omega_3 \theta_t} + \frac{\eta_1}{\omega_3 \theta_i} \right)}$$

E parallel to interface.

compare this with normal incidence:

$$\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$$

η_2 and η_1 have been replaced by the 2-directed impedances for E parallel to interface case!

Similarly, for H parallel to the interface case, η_2 and η_1 will be replaced by the 2-directed impedance appearing in eqn. (22):

$$\Gamma = \left(\frac{\eta_2 \cos \theta_t - \eta_1 \cos \theta_i}{\eta_2 \cos \theta_t + \eta_1 \cos \theta_i} \right)$$

— H parallel to interface.